

不可靠通信通道 Markovian 跳变系统的 量化分析与设计

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[摘要] 研究了具有不可靠通信通道的离散时间 markovian 跳变系统的量化控制问题. 首先, 构造离散 Lyapunov 函数, 利用矩阵不等式的凸性以及线性矩阵不等式技术, 得到具有较小保守性的稳定性条件; 其次, 根据线性矩阵不等式技术求解量化反馈控制器设计的增益, 稳定性条件和控制器增益设计最后转换成线性矩阵不等式方程的求解, 通过 matlab 可以很容易实现; 最后通过数值例子来例证所述方法的有效性.

[关键词] Markovian 跳变系统, 凸性, 信号量化

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Analysis and Design for Discrete Markovian Jump Time-Delay Systems With Unreliable Communication Channel Based on Signal Quantization

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Abstract: This paper investigates the issue of quantized controller for discrete-time markovian jump systems with unreliable communication channel. Firstly, by exploiting a discrete Lyapunov function and using the convexity property of the matrix inequality as well as Jensen inequality, new criteria are derived which are less conservative. Secondly, based on the obtained conditions, the gain of quantized controller can be easily obtained through Matlab in terms of linear matrix inequalities (LMIs). Finally, a numerical example is provided to show the effectiveness of the proposed theoretical results.

Key words: Markovian jump systems, convexity property, signal quantization

由于随机突变现象的存在,许多实际动态系统经常会出现不同结构之间的切换现象,比如电源系统、经济系统等等,通常采用以时间驱动或事件驱动机构的混杂系统模型来处理该类复杂问题.马尔科夫跳变系统(MJLS)属于混杂系统的一种,在过去几十年中,马尔科夫跳变系统的分析与综合问题取得了很多成果,文献[1]研究了时滞依赖的离散 Markovian 跳变系统的稳定性分析与 H_∞ 控制器设计,文献[2]在考虑信号传输时滞情况下研究了 Markovian 跳变系统的稳定和镇定问题,文献[3]研究了具有未知转换概率的奇异 Markovian 跳变系统的稳定及镇定问题.然而,在具有时滞的动态系统的分析中,首先假设所有的数据传输都具有无穷精度,从而忽略信号量化的影响,但是由于信号传输能力有限,信号在传输至下一节点前必须量化.最近,信号量化问题受到广泛关注,文献[4]研究了具有输出量化的线性控制系统的镇定问题,文献[5]研究了线性系统以及非线性系统的输入量化问题,文献[6]及[7]分别研究了线性系统的 H_2 及 H_∞ 量化控制问题.但是,Markovian 跳变系统的量化控制问题至今未得到关注,而实际系统的切换性和量化问题的重要性使得该方向的研究具有重要意义.

本文首次研究了具有不可靠通信通道的基于信号量化的 Markovian 跳变系统的稳定性分析及控制器设计问题,建立了更符合实际情况的离散时间 Markovian 跳变系统模型;利用两个量化器对状态输入信号

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定义 1^[12] 若对于所有 $\phi(k)$, $k = -\tau_M, -\tau_M+1, \dots, 0$, $r(k) \in h$, $k = -\tau_r, -\tau_r+1, \dots, 0$, $\mathcal{E}\{\sum_{k=0}^{\infty} \|\mathbf{x}(k; \phi(\cdot), r(\cdot))\|^2\} < \infty$ 成立, 则系统均方意义上指数稳定 (EMSS).

2 主要结果

定理 1 对于给定 $\tau_m, \tau_r > 0$ 及常数矩阵 $K_j(j \in h)$, 若存在适当维数的矩阵 $P_j(j \in h) > 0$, $Q_i > 0$, $R_i > 0$ ($i = 1, 2$), $T > 0$, N_{1i} , M_{1i} , S_i ($i = 1, \dots, 5$) 使得下列线性矩阵不等式成立, 则系统 (6) 均方意义上指数稳定:

$$\begin{bmatrix} \Gamma_{11} + T & * \\ \Gamma_{21} & -R_2 \end{bmatrix} < 0, \quad (7)$$

且量化器满足:

$$2\Delta \|\mathbf{S}B_i\| \|\mathbf{T}^{-1}\| \leq \frac{\|\mathbf{x}(k)\|}{\mu_2} \leq F_1; F_2 \geq \|\mathbf{K}_{i-\tau_r}\| (\Delta_1 + F_1), \quad (8)$$

$$\text{其中 } \Gamma_{11} = \begin{bmatrix} \Gamma_{11}^{11} & * & * & * & * \\ \mathbf{R}_1 + \mathbf{N}_{11}^T + \mathbf{S}_2 - \mathbf{S}_2 \mathbf{A}_i & \Gamma_{11}^{22} & * & * & * \\ -\mathbf{M}_{11}^T + \mathbf{S}_3 - \mathbf{S}_3 \mathbf{A}_i & -\mathbf{M}_{12}^T + \mathbf{N}_{13} & -\mathbf{Q} - \mathbf{M}_{13} - \mathbf{M}_{13}^T & * & * \\ \Gamma_{11}^{41} & \Gamma_{11}^{42} & \Gamma_{11}^{43} & \Gamma_{11}^{44} & * \\ \Gamma_{11}^{51} & \mathbf{N}_{15} + \mathbf{S}_2^T & -\mathbf{M}_{15} + \mathbf{S}_3^T & \Gamma_{11}^{54} & \Gamma_{11}^{55} \end{bmatrix}.$$

$$\Gamma_{21}^1 = [\sqrt{\delta} \mathbf{M}_{11}^T \quad \sqrt{\delta} \mathbf{M}_{12}^T \quad \sqrt{\delta} \mathbf{M}_{13}^T \quad \sqrt{\delta} \mathbf{M}_{14}^T \quad \sqrt{\delta} \mathbf{M}_{15}^T]; \Gamma_{21}^2 = [\sqrt{\delta} \mathbf{N}_{11}^T \quad \sqrt{\delta} \mathbf{N}_{12}^T \quad \sqrt{\delta} \mathbf{N}_{13}^T \quad \sqrt{\delta} \mathbf{N}_{14}^T \quad \sqrt{\delta} \mathbf{N}_{15}^T];$$

$$\Gamma_{11}^{11} = \sum_{j=1}^N \pi_{ij} P_j - P_i + Q_1 + Q_2 - R_1 + S_1 + S_1^T - S_1 A_i - A_i^T S_1^T; \Gamma_{11}^{22} = -Q_1 - R_1 + N_{12} + N_{12}^T;$$

$$\Gamma_{11}^{41} = \mathbf{M}_{11}^T - \mathbf{N}_{11}^T + \mathbf{S}_4 - \mathbf{S}_4 \mathbf{A}_i - \mathbf{K}_{i-\tau_r}^T \mathbf{B}_i^T \mathbf{S}_1^T; \Gamma_{11}^{42} = \mathbf{M}_{12}^T - \mathbf{N}_{12}^T + \mathbf{N}_{14} - \mathbf{K}_{i-\tau_r}^T \mathbf{B}_i^T \mathbf{S}_2^T; \Gamma_{11}^{43} = \mathbf{M}_{13}^T - \mathbf{M}_{14} - \mathbf{N}_{13}^T - \mathbf{K}_{i-\tau_r}^T \mathbf{B}_i^T \mathbf{S}_3^T;$$

$$\Gamma_{11}^{44} = \mathbf{M}_{14} + \mathbf{M}_{14}^T - \mathbf{N}_{14} - \mathbf{N}_{14}^T - \mathbf{K}_{i-\tau_r}^T \mathbf{B}_i^T \mathbf{S}_4^T - \mathbf{S}_4 \mathbf{B}_i \mathbf{K}_{i-\tau_r}; \Gamma_{11}^{51} = \sum_{j=1}^N \pi_{ij} P_j + \mathbf{S}_5 + \mathbf{S}_1^T - \mathbf{S}_5 \mathbf{A}_i;$$

$$\Gamma_{11}^{54} = \mathbf{M}_{15} - \mathbf{N}_{15} + \mathbf{S}_4^T - \mathbf{S}_5 \mathbf{B}_i \mathbf{K}_{i-\tau_r}; \Gamma_{11}^{55} = \sum_{j=1}^N \pi_{ij} P_j + \tau_m^2 R_1 + \delta R_2 + \mathbf{S}_5 + \mathbf{S}_5^T.$$

$$\text{证明 构造如下李亚普诺夫函数 } V(\mathbf{x}_k, \mathbf{r}(k)) = \sum_{i=1}^3 V_i(\mathbf{x}_k, \mathbf{r}(k)),$$

$$\text{其中 } V_1(\mathbf{x}_k, \mathbf{r}(k)) = \mathbf{x}^T(k) \mathbf{P}(\mathbf{r}(k)) \mathbf{x}(k); V_2(\mathbf{x}_k, \mathbf{r}(k)) = \sum_{i=k-\tau_m}^{k-1} \mathbf{x}^T(i) \mathbf{Q}_1 \mathbf{x}(i) + \sum_{i=k-\tau_M}^{k-1} \mathbf{x}^T(i) \mathbf{Q}_2 \mathbf{x}(i);$$

$$V_3(\mathbf{x}_k, \mathbf{r}(k)) = \tau_m \sum_{i=-\tau_m}^{-1} \sum_{j=k+i}^{k-1} \mathbf{y}^T(i) \mathbf{R}_1 \mathbf{y}(i) + \sum_{i=-\tau_M}^{-\tau_m-1} \sum_{j=k+i}^{k-1} \mathbf{y}^T(i) \mathbf{R}_2 \mathbf{y}(i).$$

假设 k 时刻的模式为 i , 则 $\mathbf{P}(\mathbf{r}_k) = \mathbf{P}_i$, $\mathbf{A}(\mathbf{r}_k) = \mathbf{A}_i$, $\mathbf{B}(\mathbf{r}_k) = \mathbf{B}_i$, $\mathbf{K}(\mathbf{r}_k) = \mathbf{K}_{i-\tau_r}$, $k+1$ 时刻的模式假设为 j , 定义 $\mathbf{y}(k) = \mathbf{x}(k+1) - \mathbf{x}(k)$, 则:

$$\mathcal{E} \Delta V_1(\mathbf{x}_k, \mathbf{r}(k)) = \mathbf{x}^T(k+1) \left[\sum_{j=1}^N \pi_{ij} P_j \right] \mathbf{x}(k+1) - \mathbf{x}^T(k) \mathbf{P}_i \mathbf{x}(k) = [\mathbf{x}^T(k) + \mathbf{y}^T(k)] \left[\sum_{j=1}^N \pi_{ij} P_j \right] [\mathbf{x}(k) +$$

$$\mathbf{y}(k)] - \mathbf{x}^T(k) \mathbf{P}_i \mathbf{x}(k) = 2\mathbf{x}^T(k) \sum_{j=1}^N \pi_{ij} P_j \mathbf{y}(k) + \mathbf{y}^T(k) \sum_{j=1}^N \pi_{ij} P_j \mathbf{y}(k) + \mathbf{x}^T(k) \left[\sum_{j=1}^N \pi_{ij} P_j - \mathbf{P}_i \right] \mathbf{x}(k),$$

$$\mathcal{E} \Delta V_2(\mathbf{x}_k, \mathbf{r}(k)) = \mathbf{x}^T(k) [\mathbf{Q}_1 + \mathbf{Q}_2] \mathbf{x}(k+1) - \mathbf{x}^T(k-\tau_m) \mathbf{Q}_1 \mathbf{x}(k-\tau_m) - \mathbf{x}^T(k-\tau_M) \mathbf{Q}_2 \mathbf{x}(k-\tau_M),$$

$$\mathcal{E} \Delta V_3(\mathbf{x}_k, \mathbf{r}(k)) = \mathbf{y}^T(k) [\tau_m^2 \mathbf{R}_1 + (\tau_M - \tau_m) \mathbf{R}_2] \mathbf{y}(k) - \tau_m \sum_{i=k-\tau_m}^{k-1} \mathbf{y}^T(i) \mathbf{R}_1 \mathbf{y}(i) - \sum_{i=k-\tau_M}^{k-\tau_m-1} \mathbf{y}^T(i) \mathbf{R}_2 \mathbf{y}(i).$$

运用引理 1, 可得:

$$-\tau_m \sum_{i=k-\tau_m}^{k-1} \mathbf{y}^T(i) \mathbf{R}_1 \mathbf{y}(i) \leq \begin{bmatrix} \mathbf{x}(k) \\ \mathbf{x}(k-\tau_m) \end{bmatrix}^T \begin{bmatrix} -\mathbf{R}_1 & \mathbf{R}_1 \\ \mathbf{R}_1 & -\mathbf{R}_1 \end{bmatrix} \begin{bmatrix} \mathbf{x}(k) \\ \mathbf{x}(k-\tau_m) \end{bmatrix}.$$

采用参考文献 [13] 所采用的自由权矩阵技术可得:

$$\begin{aligned}
 & 2\xi^T(k) M_1 [x(k-\tau(k)) - x(k-\tau_M) - \sum_{i=k-\tau_M}^{k-\tau(k)-1} y(i)] = 0; 2\xi^T(k) N_1 [x(k-\tau_m) - x(k-\tau(k)) - \sum_{i=k-\tau(k)}^{k-\tau_m-1} y(i)] = 0; \\
 & 2\xi^T(k) S [x(k+1) - A_i x(k) - B_i K_{i-\tau_r} x(k-\tau(k)) + B_i \mu_2 \delta; \\
 & -2\xi^T(k) M_1 \sum_{i=k-\tau_M}^{k-\tau(k)-1} y(i) \leq \sum_{i=k-\tau_M}^{k-\tau(k)-1} y^T(i) R_2 y(i) + (\tau_M - \tau(k)) \xi^T(k) M_1 R_2^{-1} M_1^T \xi(k); \\
 & -2\xi^T(k) N_1 \sum_{i=k-\tau(k)}^{k-\tau_m-1} y(i) \leq \sum_{i=k-\tau(k)}^{k-\tau_m-1} y^T(i) R_2 y(i) + (\tau(k) - \tau_m) \xi^T(k) N_1 R_2^{-1} N_1^T \xi(k); \\
 & \text{其中 } M_1^T = [M_{11}^T \ M_{12}^T \ M_{13}^T \ M_{14}^T \ M_{15}^T]; N_1^T = [N_{11}^T \ N_{12}^T \ N_{13}^T \ N_{14}^T \ N_{15}^T]; S^T = [S_1^T \ S_2^T \ S_3^T \ S_4^T \ S_5^T]; \\
 & \xi^T(k) = [x^T(k) \ x^T(k-\tau_m) \ x^T(k-\tau_M) \ x^T(k-\tau(k)) \ y(k)].
 \end{aligned}$$

根据引理 2, 可得:

$$\begin{aligned}
 & \xi^T(k) \Gamma_{11} \xi(k) + (\tau_M - \tau_m) M_1 R_2^{-1} M_1^T + 2\xi^T(k) S B_i \mu_2 \delta < 0; \\
 & \xi^T(k) \Gamma_{11} \xi(k) + (\tau_M - \tau_m) N_1 R_2^{-1} N_1^T + 2\xi^T(k) S B_i \mu_2 \delta < 0.
 \end{aligned}$$

则由定理 1 可得 $\varepsilon(\Delta V(k)) \leq -\frac{\|\xi(k)\|}{T^{-1}} (\xi(k) - 2 \|S B_i\| \mu_2 \delta \|T^{-1}\|)$, 定理 1 得证.

以下根据稳定性定理 1 设计量化反馈控制器.

定理 2 对于给定常数 $\tau_m > 0$, $\tau_M > 0$ 及标量 ρ_1, \dots, ρ_5 , 若存在 $\bar{P}_j(j\mathcal{E}h) > 0$, $\bar{Q}_i > 0$, $\bar{R}_i > 0$ ($i=1, 2$), $\bar{T} > 0$, \bar{N}_{1i} , \bar{M}_{1i} , $Y_j(j\mathcal{E}h)$ 使得下列 LMIs 成立, 则系统 (6) 均方意义下指数稳定:

$$\begin{bmatrix} \bar{T}_{11} + \bar{T} & * \\ \bar{T}_{21}^T & -\bar{R}_2 \end{bmatrix} < 0 \quad (l=1, 2), \quad (9)$$

且控制器为 $K_j = Y_j^* X^{-T}(j\mathcal{E}h)$, 量化器参数满足:

$$2\Delta \| [\rho_1 X^{-T} \ \rho_2 X^{-T} \ \rho_3 X^{-T} \ \rho_4 X^{-T} \ \rho_5 X^{-T}] B_i \| \| T^{-1} \| \leq \frac{\|x(k)\|}{\mu_2} \leq F_1; F_2 \geq \|Y_{i-\tau_r} X^{-T}\| (\Delta_1 + F_1).$$

其中,

$$\bar{T}_{11} = \begin{bmatrix} \bar{T}_{11}^{11} & * & * & * & * \\ \bar{R}_1 + \bar{N}_{11}^T + \rho_2 X^T - \rho_2 A_i X^T & \bar{T}_{11}^{22} & * & * & * \\ -\bar{M}_{11}^T + \rho_3 X^T - \rho_3 A_i X^T & -\bar{M}_{12}^T + \bar{N}_{13} & -\bar{Q} - \bar{M}_{13} - \bar{M}_{13}^T & * & * \\ \bar{T}_{11}^{41} & \bar{T}_{11}^{42} & \bar{T}_{11}^{43} & \bar{T}_{11}^{44} & * \\ \bar{T}_{11}^{51} & \bar{N}_{15} + \rho_2 X & -\bar{M}_{15} + \rho_3 X & \bar{T}_{11}^{54} & \bar{T}_{11}^{55} \end{bmatrix};$$

$$\bar{T}_{11}^{22} = -\bar{Q}_1 - \bar{R}_1 + \bar{N}_{12} + \bar{N}_{12}^T; \bar{T}_{21} = [\sqrt{\tau} \bar{M}_{11}^T \ \sqrt{\tau} \bar{M}_{12}^T \ \sqrt{\tau} \bar{M}_{13}^T \ \sqrt{\tau} \bar{M}_{14}^T \ \sqrt{\tau} \bar{M}_{15}^T];$$

$$\bar{T}_{21} = [\sqrt{\tau} \bar{N}_{11}^T \ \sqrt{\tau} \bar{N}_{12}^T \ \sqrt{\tau} \bar{N}_{13}^T \ \sqrt{\tau} \bar{N}_{14}^T \ \sqrt{\tau} \bar{N}_{15}^T]; \bar{T}_{11}^{41} = \sum_{j=1}^N \pi_{ij} \bar{P}_j - \bar{P}_i + \bar{Q}_1 + \bar{Q}_2 - \bar{R}_1 + \rho_1 X^T + \rho_1 X - \rho_1 A_i X^T - \rho_1 X A_i^T;$$

$$\bar{T}_{11}^{41} = \bar{M}_{11}^T - \bar{N}_{11}^T + \rho_4 X^T - \rho_4 A_i X^T - \rho_1 Y_{i-\tau_r}^T B_i^T; \bar{T}_{11}^{42} = \bar{M}_{12}^T - \bar{N}_{12}^T + \bar{N}_{14} - \rho_2 Y_{i-\tau_r}^T B_i^T;$$

$$\bar{T}_{11}^{43} = \bar{M}_{13}^T - \bar{M}_{14}^T - \bar{N}_{13}^T - \rho_3 Y_{i-\tau_r}^T B_i^T; \bar{T}_{11}^{44} = \bar{M}_{14}^T + \bar{M}_{14}^T - \bar{N}_{14}^T - \rho_4 Y_{i-\tau_r}^T B_i^T - \rho_4 B_i Y_{i-\tau_r};$$

$$\bar{T}_{11}^{51} = \sum_{j=1}^N \pi_{ij} \bar{P}_j + \rho_5 X^T + \rho_1 X - \rho_5 A_i X^T; \bar{T}_{11}^{54} = \bar{M}_{15} - \bar{N}_{15} + \rho_4 X - \rho_5 B_i Y_{i-\tau_r};$$

$$\bar{T}_{11}^{55} = \sum_{j=1}^N \pi_{ij} \bar{P}_j + \tau_m^2 \bar{R}_1 + (\tau_M - \tau_m) \bar{R}_2 + \rho_5 X^T + \rho_5 X.$$

证明 设 $S_i = \rho_i X^{-1}$ ($i=1, \dots, 5$) 将不等式 (7) 左乘及右乘 $\text{diag}(\overbrace{X, \dots, X}^7)$ 及其转置, 设 $\bar{P}_j(j\mathcal{E}h) > 0 = X P_j X^T(j\mathcal{E}h)$, $\bar{Q}_i = X Q_i X^T$, $\bar{R}_i = X R_i X^T$ ($i=1, 2$), $\bar{T} = X T X^T$, $\bar{N}_{1i} = X N_{1i} X^T$, $\bar{M}_{1i} = X M_{1i} X^T$, 则定理 2 得证.

3 数值例子

研究如下两模态的 Markovian 跳变系统, $\tau_r = 1$, 设定系统 (6) 参数为: $A_1 = \begin{bmatrix} 1.5 & 1 \\ 0 & 0.5 \end{bmatrix}$, $A_2 =$

$\begin{bmatrix} 0.6 & 0 \\ 0.1 & 1.2 \end{bmatrix}$, $B_1 = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$, $B_2 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$, $\pi = \begin{bmatrix} 0.1 & 0.9 \\ 0.5 & 0.5 \end{bmatrix}$, 假设 $K_1 = [-0.063 \quad -0.148 \quad 1]$, $K_2 = [-0.057 \quad 4$

$-0.139 \quad 3]$ 模态转换如图 3 所示. 根据定理 1, 应用 matlab 工具箱, 可得当 $\tau_m = 1$ 所求得的时滞上界为 $\tau_M = 5$, 而参考文献 [11] 相同条件下的时滞上界为 $\tau_M = 3$, 比较结果可以看出, 本文所采用的方法具有较小保守性. 从图 4 的响应曲线可以看出系统具有很好的稳定性.

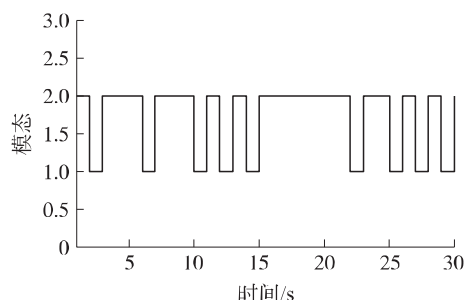


图 3 模态转换图
 Fig.3 Diagram of mode

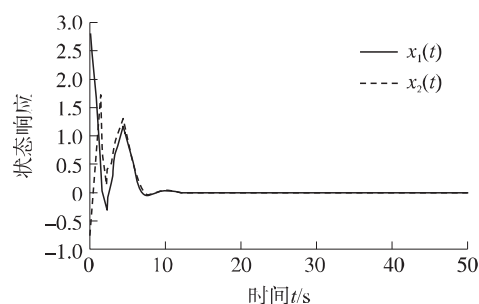


图 4 系统响应曲线
 Fig.4 State Response of the system

4 结论

本文建立了具有不可靠通信通道的离散时间 Markovian 跳变系统的模型, 并分析了该系统的稳定性, 给出了稳定性条件, 得出了量化控制器设计方法. 矩阵不等式凸性的应用以及 Jensen 不等式的引入使得本文所得的结果具有较小的保守性. 数值例子验证了本文所述方法的有效性.

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